Fifteen Years of Lessons Learned: Design and Construction of CFRP Liners for Large Diameter Pipelines

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ABSTRACT

Strengthening of p ressure pi pelines usi ng carbon fi ber rei nforced pol ymer (CFRP) materials has be en an ac cepted r epair m ethod since the late 1990's. CF RP composites are hi gh str ength, non-co rrosive and durable materials and can add considerable structural capacity which makes them very suitable for pressure pipeline strengthening. How ever, t here are seve ral keys to success and best practices with regard to ma terial se lection, de sign, construction and qualit y control. There a re lessons le arned thr ough insta llations w hich have taken pla ce over the past fifteen years. These include adoption of criteri a fo r material selection, new desig n philosophies, termination end detailing and critical points during the construction process. This pape r provides state of the art information regarding materials, de sign considerations, i nstaller experiences and current best practices. Fi eld c ase st udies provide a comprehensive review of the use of CFRP composites.

1. BACKGROUND

Over the p ast fifte en years inspection methods f or large diameter pipelines have evolved to includ e more ac curate me thods, f ailure r isk a nalysis a nd re pair prioritization. The se a dvancements ha ve pr ovided utilit y ow ners w ith c ritical information regarding the exact location of distressed pipes and caused an increase in demand for targeted rehabilitation technolog ies. Based on th is repair prioritization information, utilities have taken proactive steps in a dvance of failure to replace or repair the distressed pipes with an unacceptably high risk of failure. There are several repair options for concrete pressure pipes which include encasing the degraded pipe in a reinforced concrete block, post-tensioning by wrapping tendons around the pipe, or relining the pipeline. Relining is typically performed by utilizing CFRP or by steel slip lining.

CFRP was first used in the United States for the internal rehabilitation and strengthening of Pre-Stressed Concrete C ylinder Pipe (PCCP) in the late 1990s. The use of internally applied CFRP is applicable to pipelines 30 inch diameter and above because manned entry is required into the pipeline for application of CFRP materials. Following the initia l insta llations, a nd a n e valuation pe riod, va rious munic ipal pipeline owners and power generation stations began to use C FRP lining for PCCP on a regular basis. By the mid- 2000s, insta llation of CFRP on the interior of PCCP had become a widely acceptable repair and strengthening system for PCCP.

CFRP lining system design principles have also evolved since the first repairs took place in the 1990s, and through testing and experience, improvements in design concepts have led to an increase in the long term performance expectations for CFRP systems (McRe ynolds et al, 2013). The re is currently no standard for design and installation of CF RP lining re pairs of pipe s. T here is a n A merican Wa ter Works Association (AWWA) subcommittee which is in the process of developing a standard which addresses design, materials, installation, and quality control for CFRP upgrade (repair, str engthening) of PCCP (ANSI/AWWA CF RP). The d esign pr inciples described below are in line with the standard being developed by AWWA.

In the past 10 years CFRP has been a dopted for use in man y other t ypes of pipe structures as well including steel, mortar lined steel and polymer pipes. This paper focuses on the use of CF RP for PCCP, a s that is its most c ommon pipeline application.

2. MATERIAL SELECTION

A typical CFRP lining system consists of a primer, thickened epoxy, epoxy, reinforcing fabric, and top coat. The most effective epoxy systems for long-term civil infrastructure r ehabilitation a pplications, such a sr ehabilitation of P CCP line s, a re ambient cure thermoset epoxy systems. In order to minim ize environmental haz ards present inside the pipeli ne during application of the materials, epoxy systems which are made of 100% solids and are Volatile Organic Compoud (VOC) compliant are utilized. The primer lay er of e poxy a pplied to the pipe consists of a low visc osity epoxy as shown in Figure 1 which penetrates into the concrete substrate, providing an adhesive bond for the thickened epoxy and saturating layers as well as subsequent layers of the CF RP s ystem. The thickened e poxy s ystem is made up of e ither a specially form ulated higher viscosity epoxy s ystem or made up of the saturating epoxy and silic a f ume which have b een mix ed tog ether in a ccordance w ith the manufacturer's recommended procedure. The thickened epoxy filler is used to even out the concrete substrate, fill voids and it is also used in between layers of CFRP to ensure intimate contact of the CFRP system at all locations within the CFRP liner.

The t op coat of t he C FRP is typically m ade of thickened epox y, with or without a pig ment add ed for eas e of identific ation of repaired pipes egment(s). In environments where high concentrations of H2S or aggressive chemicals are utilized, a top coat with high chemical resistance is used. In circumstances where the CFRP system i s appl ied ex ternally t o ex posed pi ping, a UV r esistant t op coat i s recommended. In c ases where potable wa ter is conve yed by the pipeline s ystem, industry standard is that all materials utili zed in the CF RP liner repair have been tested to be in c ompliance with A NSI/NSF 61, which is the nationally recognized health eff ects standard f or all component s, devi ces, and mat erials which come in contact with drinking water (ANSI/NSF, 2013).



Figure 1. Application of epoxy primer

2.1 Types of FRP composites used

There are a wide variety of reinforcing fabrics available, however for internal repair of pipelines b est practices include only the use of unidirectional carbon fiber fabric as structural reinforcement. In order to resist all of the design loads acting on the pipeline, sep arate s heets of unidirectional carbon fiber reinforcing fabric a re applied to the interior of the pipeline with the direction of the fibers oriented in either the long itudinal or the circumferential direction to pr ovide the ne cessary strength. Carbon fibe rs have the potential for relectrical conductivity; therefore, to avoid galvanic corrosion of steel in proximity to carbon fibers, a g lass fiber f abric is use d for isolation of any steel substrate from the CFRP system.

2.2 Material performance requirements

Unlike traditional construction materials such as concrete and steel, for CFRP liner systems, the selection of appropriately functional and durable CFRP materials is placed on the owner or engineer. Num erous materials available in the market have different short and long term properties in the exposure environment, and it is the responsibility of the owners, engineers and material suppliers to perform the necessary tests to demonstrate that the materials have the necessary reliability and

durability. Material resistance adjustment factors, used in design along with load factors, need to be based on the sufficiently large number of test samples tested in accordance with a number of short and long term test methods. If unsuitable FRP materials are installed, this could result in a substantial reduction in the service life of the pipeline(s) where CFRP is installed.

One industry certification aids owners and engineers is the inclusion of a valid International Code Council (ICC) Evaluation Service Report (ESR) as a requirement for F RP ma terials. ICC de veloped a set of m inimum dur ability and p erformance criteria for C FRP m aterials which m ust be ad hered t o i n order t o recei ve ICC approval and a valid ICC report. ICC's Acceptance Criteria 125 (AC125) and AC178 establish the mini mum acceptable dur ability c riteria, str uctural pe rformance, a nd inspection cri teria for a ny C FRP s ystem t o be consi dered sui table for st ructural rehabilitation a pplications. To obta in a v alid ICC Re port, ma terials mu st ma intain minimum percent retention of properties when they are tested after 1,000 hour, 3,000 hour, and 10,000 hour exposure to various a ggressive environments inclu ding water at different temperatures, saltwater, alkali solutions, and dry heat (ICC 125, 2010 and ICC 178, 2010). Speci fications which p rotect owners and en gineers, ensuring properly tested CFRP materials are installed, require a valid ICC report b e provided as part of the bid submission.

More ex tensive dur ability testin g b eyond the 10,000 hour exposure tests required by ICC AC125 are available for selected CFRP materials. For instance, a recent study was released which highlights an 8-year (70,000 hour) durability study completed by the Metropolitan Water District of Southern California (Sleeper et al, 2010). In this stud y, an inspection of CF RP lined PC CP was performed approximately eight years after the installation of the CFRP lining system. The visual and sounding inspection indicated no damage in the form for delaminations, bubbles, cracks, or ed gelifting. Observations from the sam e inspectors who we represent during the initial CF RP lining installation noted that the CF RP was in c omparable condition to the originally installed system. In addition to the results of the in-service CFRP inspection, coupo ns made from the same CFRP system installed in MW D's pipeline w ere te nsile te sted a fter e ight years of e xposure to ta p w ater in environmental chambers. The tensile test results indicated minimal change in the structural performance of the C FRP system, as measured through tensile strength, tensile modulus and breakage strain, after being continuously immersed in tap water for a period of over eight years (Sleeper et al, 2010). The results of this durability study indicate strong potential for the CF RP lining system to perform well as a longterm solution for pipeline rehabilitation.

3. CFRP LINER DESIGN

The circumferential design of a CFRP liner is based on the combined effects of gravity loads and internal pressures consisting of pipe and fluid weights and earth load that will be imparted to the lined pipe as the host pipe continues to deteriorate and experiences degradation. For a distressed or degraded PCCP, the CFRP liner can be designed as a composite system with the inner concrete core or as a stand-alone system which does not rely on the host pipe for resisting any of the design loads. Levels of degradation of the host pipe at the time of installation are discussed below, and in most cas es, the host pipe is expected to continue to deteriorate with time such t hat the C FRP s ystem needs t o be d esigned for the expected host pipe condition at the end of the service life.

- Non-Degraded Pipe. The CF RP liner for a non-degraded pipe, requiring strengthening due to increased load (e.g., pressure, earth load, live load), is designed by considering the composite action of the C FRP with the entire pipe wall thickness.
- Degraded Pipe. A de graded pipe consis ts of PCCP with broken wires, but with an inner core that is circular and may have some minor cracking that can be repaired.
- Severely De graded Pipe. Severel y de graded p ipe c onsists of PC CP with broken w ires, multiple w ide cr acks in the concrete c ore a s w ell as a significantly deformed and uneven internal surface with ovality or waviness imperfection.

CFRP r epair of de graded PCC P is de signed to provide str ength, dura bility, and r eliability thr oughout the service life of the repaired pipe when the pipe line is subjected to long-term and short-term loads. The CFRP system, as shown in Figure 2 is to have adequate reliability such that the probability of failure of the repaired pipe resulting from the variations of loads and resistance is similar to the probability of failure a ssociated w ith the use of mor e tr aditional str uctural r epair m aterials or pipeline replacement.



Figure 2. Completed CFRP lined section prior to removal of scaffolding

3.1 Structural behavior of CFRP liner for degraded PCCP

While a pplied loa ds do not c hange si gnificantly ov er time, the mome nt capacity of t he pi pe reduces as t he rep aired pi pe de grades due t o i ncrease i n t he

number of broken pr estressing wires and cracking of the core. The structural system of the pipe changes from a relatively rigid pipe at the time of internal repair, to a more fl exible, fully det eriorated pipe resulting in inc reased d effections and pipe ovaling. The CFRP system has to be capable of accommodating such deformations.

The design of the CF RP liner is based on the loss of all prestressing wires which results in a flex ible pipe design for the liner. In addition, the design accounts for the bending of the CFRP lining due to differential stiffness along the length of the pipe encountered d uring the degradation p rocess, as ther e will be localized wire breaks (in the form of bands) which cause differences in stiffness along the length of the pipe. Like other flexible pipe designs, the CFRP liner relies on the stiffness of the soil to resist the external loads. Adequate geotechnical data at the site is needed to support selection of the cons trained soil modulus for desig n of the CF RP liner (AWWA M45).

3.2 Design limit states

As part of the process of CFRP lining design, multiple limit states must be addressed. For a stand-alone C FRP liner design, the limit states addressed are as follows:

- Rupture of CF RP c ircumferential a nd lon gitudinal la minate in tension, compression, flexure, or shear.
- Circumferential or longitudinal buckling of the CFRP laminate.

When the inner concrete core is taken into account in the CFRP design, the following additional limit states are addressed:

- Rupture of the CFRP laminate in tension or combined tension and bending.
- Buckling of the CFRP laminate bonded to concrete inner core.
- Debonding of CFRP from the concrete inner core under one of the following circumstances:
 - Shear between the CFRP and the concrete inner core.
 - Excessive radial tension.
 - Concrete core crushing from gravity loads, in absence of i nternal pressure.

All applicable limit states must be accounted f or in the CF RP design in coordination with appr opriate loading combinations and material adjustment factors such that a conservative CFRP lining design is developed.

4. CFRP LINER INSTALLATION

CFRP r epair of la rge diameter PCCP l ines require ex tensive planning, especially in municipal areas where traffic control and ot her complications persist. Dewatering and access to pipeline segments to be repaired are typically coordinated by the Owner. Prior to the pipeline shutdown period crews ar rive at the site; set up fencing and material, equipment, and stor age ar eas, te mporary office fa cilities a s

necessary, la y-down ar eas, and satur ator a nd m aterial mix ing are as; and have all required mate rials and e quipment stag ed at the pipeline w ork loc ations. A typical enclosed mixing area is shown below, in Figure 3. The mixing and storage areas for materials must be maintained at a minimum temperature of 40F.



Figure 3. Typical enclosed material mixing area

Safety is an important aspect of these projects, given that the work takes place in a confined spa ce with limited access and egress availability. Ensuring that crews within the pipe h ave adequate air supply is o ne portion of the s afety approach. Dehumidification a ir-blowing units are insta lled at the appropriate lo cations, a s shown in F igure 4, to ensure a constant supply of clean dry air for ventilation purposes and also to a ssist in drying the segments to be strengthened following the surface preparation operation.



Figure 4. Dehumidification unit

4.1 Installation procedure

General w ork ac tivities a ssociated w ith the PCCP str engthening s ystem installation that occur outside of the pipe include the preparation and mix ing of the epoxy system and the saturation of glass and carbon fabric sheets prior to mobilizing

the saturated she ets into the pipe for technician installation. Saturation takes place using specialized mechanical saturation equipment, as shown in F igure 5. F abric saturation is a critical st ep in the process and it should be even through the fabric thickness such that there are no dry fabric spots.



Figure 5. Mechanical saturator

General work activities associated with the CFRP system installation that will occur inside of the pipe include joint prep aration, surface preparation of the inner core, installation of the CFRP system, and installation of the end terminations.

4.2 Surface preparation

Surface pr eparation i s one of t he m ost im portant aspect s of t he C FRP installation process. Concrete surfaces are to be prepared to an ICRI profile of CSP-3 or greater to create an open pore structure and to remove all protrusions, sharp edges, and surface contaminants. J oint areas are also prepared during surface preparation. The steel surfaces at termination detail areas in the joints are prepared to a near-white or w hite me tal f inish, which r equires a brasive bl asting of t he st eel s ubstrate t o achieve the necessary profile.

Surface preparation can be perform ed by ultra-high pressure water blasting, abrasive blastin g or pn eumatic spong e-blasting. If wate r blasting is sel ected, it is recommended th at 40,0 00 PS I equipment, ope rating at 30,000 to 36,000 PS I is utilized to e nsure proper profile of the concrete substrate is ac complished. U se of low pressure ma y result in inadequate surfac e p reparation and low bond streng th. Abrasive blasting is ano ther effective me thod for surfac e preparation and standard techniques appl y, t o t he spe cified sur face p rofile. S pecial p recautions re garding mitigating airborne particulate levels are taken for this type of blasting in a confined space. An alternative method of abrasive blasting with envir onmental benefit is sponge-blasting, as sho wn in F igure 6. Sponge media is open- celled, water based polyurethane impregnated with abrasives.



Figure 6. Sponge-blast set-up on pipe interior

On impact with the surface, the sponge particles compress and slide across the surface producin g a s crubbing action, mo re similar to a sanding effect, but eliminating the harsher and dust y negative effects associated with conventional grit blasting. The abr asive p articles achi eve t he desi red surface pro file and the m edia rebounds at quite low v elocity as the media converts the majorit y of its e nergy into work at the surface. The sponge blast media generates less than 10% of the airborne dust levels normally experienced with conventional grit blasting medias, allowing for improved safety during surface preparation.

4.4 Installation of saturated carbon fiber system

Following the surface p reparation and prior to CFRP installation, por table scaffolding is erected, as needed, spanning the pipe section to be lined. This gives the crew the ability to apply the CF RP liner to all areas of the pipe section without the need to walk on the pipe. Best industry practice to ensure a successful installation is that the application take place continuous in a manner which avoids contact with the CFRP after installed until cured.

The saturated carbon fiber is applied to the inside surface of host pipe in a wet lay-up process. Dry layup process should not be used as it may result in unsaturated fabric and debonding. The wet- out fabric is pressed to the inside surface of the host pipe to achi eve i ntimate cont act. An y ent rapped ai r bet ween l ayers is r eleased or rolled out without wrinkling of carbon fibers. Figure 7 below shows the first layer of longitudinally applied CFRP being installed inside the pipeline.



Figure 7. Installation of longitudinal layer of CFRP

The installed carbon fiber fabric should be oriented in the directions indicated on the desig n drawings, with no g reater than 5 degree misali gnment of the fabrics from the specified direction. When the CFRP is not pr operly aligned, the affected layer of CFRP system needs to be removed and replaced prior to curing. If the CFRP layer c annot be removed without affecting the integrity of the su rrounding c arbon fiber, an additional la yer is overlaid onto the off a xis fibers to r estore the laminate structure to its intended directional strength requirements.

4.5 Termination of carbon fiber system

The termination points of the CFRP liner are designed such that internal water pressure is not able to migrate be hind the inner c ore. If the CFRP is n ot properly sealed at termination points and pressure is allowed to build up behind the inner core, the CF RP lining will be str ess-free and str ucturally in effective. Designs which include termination details with the CFRP extended into the ne xt pipe section will allow wat er pr essure t o build up behind the inner core when t he adj acent pipe degrades and hence this termination detail is no longer used.

The length of the bond b etween CFRP laminate and the steel substrat e in the joints is de signed so that the maximum axial force in the CFRP in the longitudinal direction from all loading conditions will not cause shear bond failure e or tension failure. To prevent galvanic corrosion, the CFRP is constructed on GFRP applied to steel surface. The procedure used for preparation of termination detail must avoid damage to the steel cylinder. Any damage, including gouges and punctures, needs to be repaired prior to CFRP system installation. Installation of the CFRP system into the joint region is shown in Figure 8.



Figure 8. Completed termination detail

5. QUALITY CONTROL BEST PRACTICES

The ove rall quality of CF RP line r r epairs is g overned by quality and conservatism of d esign, quality and dur ability of materials use d, experience of workers and supervisor s involved in installation, and quality of installation that includes surface preparation, mixing of epoxy, wetting carbon fiber fabric layers and installation of wetted layers and curing. Quality of CFRP installation is insured by inspection throughout the installation and inspection of the finished system. A trained Quality Control supervisor needs to observe all aspects of the onsite preparation and material application.

The CF RP installer should provide for inspection hold points to al low inspection of the workm anship of in-process construction. Inspection hold points are critical breaks in a ctivities to inspect the workmanship of in-process construction. The following steps should be independently observed by the Owner's inspector:

- Verify construction according to drawings and specifications
- Verify materials and storage conditions (expiration dates, storage temps)
- Document condition of host pipe
- Verify surface preparation and pipe cleanliness prior to CFRP installation
- Verify joint preparation
- Observe testing of mockup panels per ASTM D4541 bond testing
- Document proper control of air flow, temperature, and humidity
- Observe material preparation (fabric/epoxy weight ratios, saturator gaps)
- Observe application of CFRP (layer orientation and sequence, timing)
- Observe installation of CFRP termination details
- Observe preparation of witness panels for ASTM D3039 tensile testing
- Document curing of the CFRP system (85% cure before service)

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Perform post-installation inspection (when CFRP system is tack free)

Due to the c omplexity of the CF RP lining process, ow ner's inspec tor overseeing QA/QC for CFRP lining systems should have extensive experience in this field to ensure appropriate oversight.

5.1 Adhesion (bond strength) testing

In order to validate the adequacy of the surface preparation and the adhesion strength of the carbon fi ber strengthening system, the installer is to perform adhesion tests on t he prepared c oncrete substrate adj acent t o repair. These area s are t o be cleaned, prep ared, and covered with C FRP s ystem t est pat ches with m inimum dimensions of 2 ft x 2 ft. The patch, as shown below in F igure 9, cons ists of tw o orthogonal la yers of CF RP. Three adhe sion tests are performed and r eported in accordance with ASTM D4541. The remaining adhesion test panels are finish coated and remain in place for future testing purposes as needed.



Figure 9. ASTM D4541 bond test typical patch

5.2 Tensile testing

In order to verify the material properties of the field applied CFRP system are in line w ith the pr operties use d in the de sign, te nsile te sts a re pe rformed in accordance with AS TM D3039 on test panels which are field fabricated using the carbon fiber f abric, epoxy and saturation equipment used in the production runs for the field-installed CF RP lining s ystem. The sepa nels a re made w ith minimum dimensions of 12in. by 12 in. and are prepared on a smooth flat surface overlaid with plastic (polyethylene or vinyl) sheeting (Figure 10).

Saturating epoxy is used to prime the surface, followed by the saturated CFRP fabric, and finally topped with more saturating epoxy. A cover of plastic sheeting is placed over the panel and the panel sque egeed to remove an y bubbles and other surface irregularities to insure a smooth flat surface. The panel is labeled with time, date, sample panel numb er, fabric lot numbers, a nd epoxy batch numbers. It is then

stored in a cl ean and d ry place to cure. Two test panels are typically fabricated per day of insta llation of t he CF RP s ystem in the field. A minimum of 10% of all fabricated samples are typically tested at an independent testing laboratory. The test lab will perform tensile tests with the fibers oriented in the strong direction for each tensile test panel in accordance with ASTM D 3039 and provide tests results for tensile streng th, tensile modulus and related specime n thickness, and percent elongation.



Figure 10. ASTM D3039 Tensile Testing panel preparation

6. CONCLUSION

The desi gn and construction practic es for CF RP line rs have made significant advances throughout the past 15 years, and this paper describes the current state-of-the-art and best practices. Use of C FRP materials has become a st andard repair method for owners of large diameter pipelines, and it is anticipated that CF RP will continue to be more prevalently use d for pro-active renewal of c ritical pipe line systems. The repair system is comprised of materials that need to have tested short and long term properties with known material strength reduction factors, design that has to take into account existing and future pipe condition and all associated design limit states, experienced installers, and experienced construction quality control.

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